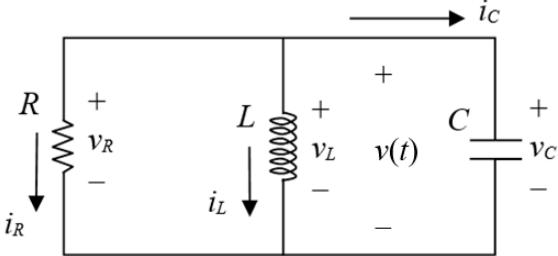


Chap 4 High Order Linear Circuits

4.1 Second-order RLC circuits without any sources

4.1.1 Parallel RLC circuit without any sources



- Component equations with initial conditions i_{L0} and v_{C0} :

$$(4.1.1-1) \quad i_R(t) = \frac{v(t)}{R}, \quad i_L(t) = \frac{1}{L} \int_0^t v(\tau) d\tau + i_{L0}, \quad i_C(t) = Cv'(t)$$

- Mathematic model

$$(4.1.1-2) \quad v_R(t) = v_L(t) = v_C(t) = v(t)$$

$$(4.1.1-3) \quad i_R(t) + i_L(t) + i_C(t) = \frac{v(t)}{R} + \frac{1}{L} \int_0^t v(\tau) d\tau + i_{L0} + Cv'(t) = 0$$

$$\Rightarrow \frac{\hat{v}(s)}{R} + \frac{1}{sL} \hat{v}(s) + \frac{i_{L0}}{s} + sC\hat{v}(s) - Cv_{C0} = 0$$

Hence, we have

$$(4.1.1-4) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0}}{C}}{s^2 + \frac{s}{RC} + \frac{1}{LC}} = \frac{sv_{C0} - \frac{i_{L0}}{C}}{s^2 + 2\alpha s + \omega_0^2} = \frac{sv_{C0} - \frac{i_{L0}}{C}}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$\text{where } \alpha = \frac{1}{2RC}, \quad \omega_0 = \frac{1}{\sqrt{LC}} \quad \text{and} \quad \xi = \frac{\alpha}{\omega_0} = \frac{1}{2R} \sqrt{\frac{L}{C}}.$$

- Characteristic roots λ_1 and λ_2

The characteristic equation is $s^2 + 2\xi\omega_0 s + \omega_0^2 = (s - \lambda_1)(s - \lambda_2)$ and thus

$$(4.1.1-5) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0}}{C}}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{sv_{C0} - \frac{i_{L0}}{C}}{(s - \lambda_1)(s - \lambda_2)}$$

where $\lambda_1, \lambda_2 = (-\xi \pm \sqrt{\xi^2 - 1})\omega_0$ are the characteristic roots.

- [A] $\xi = \frac{1}{2R} \sqrt{\frac{L}{C}} > 1$

That means $\lambda_2 < \lambda_1 < 0$ and

$$(4.1.1-6) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0}}{C}}{(s - \lambda_1)(s - \lambda_2)} = \frac{A_1}{s - \lambda_1} + \frac{A_2}{s - \lambda_2}$$

$$\Rightarrow v(t) = A_1 e^{\lambda_1 t} + A_2 e^{\lambda_2 t}$$

where $A_1 = \frac{\lambda_1}{\lambda_1 - \lambda_2} v_{C0} - \frac{1}{\lambda_1 - \lambda_2} \frac{i_{L0}}{C}$ and $A_2 = -\frac{\lambda_2}{\lambda_1 - \lambda_2} v_{C0} + \frac{1}{\lambda_1 - \lambda_2} \frac{i_{L0}}{C}$.

- [B] $\xi = \frac{1}{2R} \sqrt{\frac{L}{C}} = 1$

That means $\lambda_2 = \lambda_1 = -\xi\omega_0 = -\alpha$ and

$$(4.1.1-7) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0}}{C}}{(s + \alpha)^2} = \frac{B_1}{s + \alpha} + \frac{B_2}{(s + \alpha)^2}$$

$$\Rightarrow v(t) = (B_1 + B_2 t) e^{-\alpha t}$$

where $B_1 = v_{C0}$ and $B_2 = -v_{C0}\alpha - \frac{i_{L0}}{C}$.

- [C] $\xi = \frac{1}{2R} \sqrt{\frac{L}{C}} < 1$

That means $\lambda_1, \lambda_2 = \left(-\xi \pm j\sqrt{1 - \xi^2} \right) \omega_0 = -\alpha \pm j\beta$ and

$$(4.1.1-8) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0}}{C}}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{(s + \alpha)D_1 + \beta D_2}{(s + \alpha)^2 + \beta^2}$$

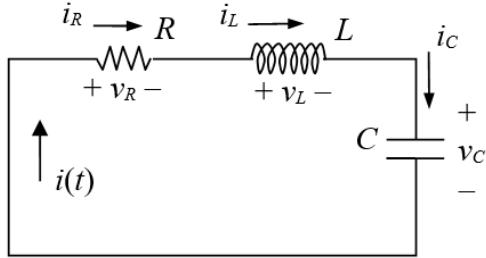
$$\Rightarrow v(t) = e^{-\alpha t} (D_1 \cos \beta t + D_2 \sin \beta t)$$

where $D_1 = v_{C0}$ and $D_2 = -\frac{\alpha v_{C0}}{\beta} - \frac{i_{L0}}{\beta C}$.

- From (4.1.1-1) and $v(t)$, we can obtain the currents through R , L and C .

Example: Consider a second-order parallel RLC circuit without any source. If $R = 4 \Omega$, $L = 2 \text{ H}$, and $C = 0.125 \text{ F}$, determine $v(t)$ and $i_C(t)$ for $t \geq 0$ when $v(0) = 1 \text{ V}$ and $i(0) = -1 \text{ A}$.

4.1.2 Series RLC circuit without any sources



- Component equations with initial conditions i_{L0} and v_{C0} :

$$(4.1.2-1) \quad v_R(t) = Ri(t), \quad v_L(t) = Li'(t), \quad v_C(t) = \frac{1}{C} \int_0^t i(\tau) d\tau + v_{C0}$$

- Mathematic model

$$(4.1.2-2) \quad i_R(t) = i_L(t) = i_C(t) = i(t)$$

$$(4.1.2-3) \quad v_R(t) + v_L(t) + v_C(t) = Ri(t) + Li'(t) + \frac{1}{C} \int_0^t i(\tau) d\tau + v_{C0} = 0$$

$$\Rightarrow R\hat{i}(s) + sL\hat{i}(s) - Li_{L0} + \frac{1}{sC}\hat{i}(s) + \frac{v_{C0}}{s} = 0$$

Hence, we have

$$(4.1.2-4) \quad \hat{i}(s) = \frac{s\hat{i}_{L0} - v_{C0}/L}{s^2 + \frac{R}{L}s + \frac{1}{LC}} = \frac{s\hat{i}_{L0} - v_{C0}/L}{s^2 + 2\alpha s + \omega_0^2} = \frac{s\hat{i}_{L0} - v_{C0}/L}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$\text{where } \alpha = \frac{R}{2L}, \quad \omega_0 = \frac{1}{\sqrt{LC}} \quad \text{and} \quad \xi = \frac{\alpha}{\omega_0} = \frac{R}{2} \sqrt{\frac{C}{L}}.$$

- Characteristic roots λ_1 and λ_2

The characteristic equation is $s^2 + 2\xi\omega_0 s + \omega_0^2 = (s - \lambda_1)(s - \lambda_2)$ and thus

$$(4.1.2-5) \quad \hat{i}(s) = \frac{s\hat{i}_{L0} - \frac{v_{C0}}{L}}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{s\hat{i}_{L0} - \frac{v_{C0}}{L}}{(s - \lambda_1)(s - \lambda_2)}$$

where $\lambda_1, \lambda_2 = (-\xi \pm \sqrt{\xi^2 - 1})\omega_0$ are the characteristic roots.

- [A] $\xi = \frac{R}{2} \sqrt{\frac{C}{L}} > 1$

That means $\lambda_2 < \lambda_1 < 0$ and

$$(4.1.2-6) \quad \hat{i}(s) = \frac{s\hat{i}_{L0} - \frac{v_{C0}}{L}}{(s - \lambda_1)(s - \lambda_2)} = \frac{A_1}{s - \lambda_1} + \frac{A_2}{s - \lambda_2}$$

$$\Rightarrow i(t) = A_1 e^{\lambda_1 t} + A_2 e^{\lambda_2 t}$$

where $A_1 = \frac{\lambda_1}{\lambda_1 - \lambda_2} i_{L0} - \frac{1}{\lambda_1 - \lambda_2} \frac{v_{C0}}{L}$ and $A_2 = -\frac{\lambda_2}{\lambda_1 - \lambda_2} i_{L0} + \frac{1}{\lambda_1 - \lambda_2} \frac{v_{C0}}{L}$.

- [B] $\xi = \frac{R}{2} \sqrt{\frac{C}{L}} = 1$

That means $\lambda_2 = \lambda_1 = -\xi\omega_0 = -\alpha$ and

$$(4.1.2-7) \quad \hat{i}(s) = \frac{s i_{L0} - \frac{v_{C0}}{L}}{(s + \alpha)^2} = \frac{B_1}{s + \alpha} + \frac{B_2}{(s + \alpha)^2}$$

$$\Rightarrow i(t) = (B_1 + B_2 t) e^{-\alpha t}$$

where $B_1 = i_{L0}$ and $B_2 = -i_{L0}\alpha - \frac{v_{C0}}{L}$.

- [C] $\xi = \frac{R}{2} \sqrt{\frac{C}{L}} < 1$

That means $\lambda_1, \lambda_2 = (-\xi \pm j\sqrt{1-\xi^2})\omega_0 = -\alpha \pm j\beta$ and

$$(4.1.2-8) \quad \hat{i}(s) = \frac{s i_{L0} - \frac{v_{C0}}{L}}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{(s + \alpha)D_1 + \beta D_2}{(s + \alpha)^2 + \beta^2}$$

$$\Rightarrow i(t) = e^{-\alpha t} (D_1 \cos \beta t + D_2 \sin \beta t)$$

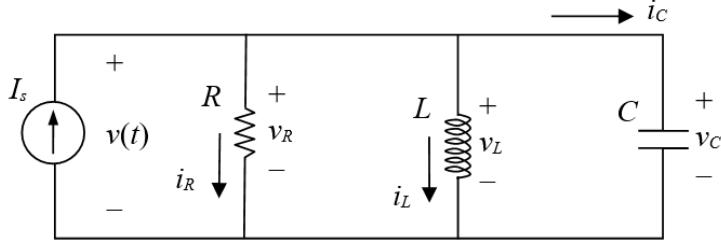
where $D_1 = i_{L0}$ and $D_2 = -\frac{\alpha i_{L0}}{\beta} - \frac{v_{C0}}{\beta L}$.

- From (4.1.2-1) and $i(t)$, we can obtain the voltages across R , L and C .

Example: Consider a second-order series RLC circuit without any source. If $R = 4 \Omega$, $L = 2 \text{ H}$, and $C = 0.125 \text{ F}$, determine $i(t)$ and $v_L(t)$ for $t \geq 0$ when $v(0) = 1 \text{ V}$ and $i(0) = -1 \text{ A}$.

4.2 Second-order RLC circuits with independent sources

4.2.1 Parallel RLC circuit with constant source



- Component equations with initial conditions i_{L0} and v_{C0} :

$$(4.2.1-1) \quad i_R(t) = \frac{v(t)}{R}, \quad i_L(t) = \frac{1}{L} \int_0^t v(\tau) d\tau + i_{L0}, \quad i_C(t) = Cv'(t)$$

- Mathematic model

$$(4.2.1-2) \quad v_R(t) = v_L(t) = v_C(t) = v(t)$$

$$(4.2.1-3) \quad i_R(t) + i_L(t) + i_C(t) = \frac{v(t)}{R} + \frac{1}{L} \int_0^t v(\tau) d\tau + i_{L0} + Cv'(t) = I_s$$

$$\Rightarrow \frac{\hat{v}(s)}{R} + \frac{1}{sL} \hat{v}(s) + \frac{i_{L0}}{s} + sC\hat{v}(s) - Cv_{C0} = \frac{I_s}{s}$$

Hence, we have

$$(4.2.1-4) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0} - I_s}{C}}{\frac{s}{s^2 + 2\alpha s + \omega_0^2} + \frac{1}{LC}} = \frac{sv_{C0} - \frac{i_{L0} - I_s}{C}}{s^2 + 2\alpha s + \omega_0^2} = \frac{sv_{C0} - \frac{i_{L0} - I_s}{C}}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$\text{where } \alpha = \frac{1}{2RC}, \quad \omega_0 = \frac{1}{\sqrt{LC}} \quad \text{and} \quad \xi = \frac{\alpha}{\omega_0} = \frac{1}{2R} \sqrt{\frac{L}{C}}.$$

- Characteristic roots λ_1 and λ_2

The characteristic equation is $s^2 + 2\xi\omega_0 s + \omega_0^2 = (s - \lambda_1)(s - \lambda_2)$ and thus

$$(4.2.1-5) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0} - I_s}{C}}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{sv_{C0} - \frac{i_{L0} - I_s}{C}}{(s - \lambda_1)(s - \lambda_2)}$$

where $\lambda_1, \lambda_2 = (-\xi \pm \sqrt{\xi^2 - 1})\omega_0$ are the characteristic roots.

- [A] $\xi = \frac{1}{2R} \sqrt{\frac{L}{C}} > 1$

That means $\lambda_2 < \lambda_1 < 0$ and

$$(4.2.1-6) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0} - I_s}{C}}{(s - \lambda_1)(s - \lambda_2)} = \frac{A_1}{s - \lambda_1} + \frac{A_2}{s - \lambda_2}$$

$$\Rightarrow v(t) = A_1 e^{\lambda_1 t} + A_2 e^{\lambda_2 t}$$

where $A_1 = \frac{\lambda_1 v_{C0}}{\lambda_1 - \lambda_2} - \frac{1}{\lambda_1 - \lambda_2} \frac{i_{L0} - I_s}{C}$ and $A_2 = -\frac{\lambda_2 v_{C0}}{\lambda_1 - \lambda_2} + \frac{1}{\lambda_1 - \lambda_2} \frac{i_{L0} - I_s}{C}$.

- [B] $\xi = \frac{1}{2R} \sqrt{\frac{L}{C}} = 1$

That means $\lambda_2 = \lambda_1 = -\xi \omega_0 = -\alpha$ and

$$(4.2.1-7) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0} - I_s}{C}}{(s + \alpha)^2} = \frac{B_1}{s + \alpha} + \frac{B_2}{(s + \alpha)^2}$$

$$\Rightarrow v(t) = (B_1 + B_2 t) e^{-\alpha t}$$

where $B_1 = v_{C0}$ and $B_2 = -v_{C0} \alpha - \frac{i_{L0} - I_s}{C}$.

- [C] $\xi = \frac{1}{2R} \sqrt{\frac{L}{C}} < 1$

That means $\lambda_1, \lambda_2 = \left(-\xi \pm j\sqrt{1 - \xi^2} \right) \omega_0 = -\alpha \pm j\beta$ and

$$(4.2.1-8) \quad \hat{v}(s) = \frac{sv_{C0} - \frac{i_{L0} - I_s}{C}}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{(s + \alpha)D_1 + \beta D_2}{(s + \alpha)^2 + \beta^2}$$

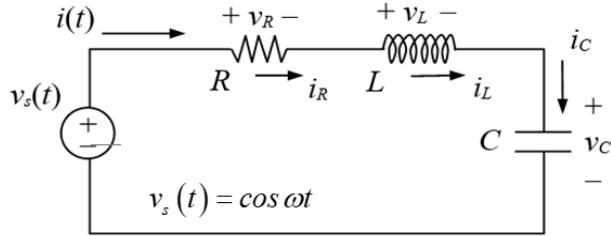
$$\Rightarrow v(t) = e^{-\alpha t} (D_1 \cos \beta t + D_2 \sin \beta t)$$

where $D_1 = v_{C0}$ and $D_2 = -\frac{\alpha v_{C0}}{\beta} - \frac{i_{L0} - I_s}{\beta C}$.

- From (4.2.1-1) and $v(t)$, we can obtain the currents through R , L and C .

Example: Consider a second-order parallel RLC circuit with independent current source $I_s = 2 \text{ A}$. If $R = 4 \Omega$, $L = 2 \text{ H}$, and $C = 0.125 \text{ F}$, determine $v(t)$ and $i_C(t)$ for $t \geq 0$ when $v(0) = 1 \text{ V}$ and $i(0) = -1 \text{ A}$.

4.2.2 Series RLC circuit with voltage source



- Component equations with initial conditions i_{L0} and v_{C0} :

$$(4.2.2-1) \quad v_R(t) = Ri(t), \quad v_L(t) = Li'(t), \quad v_C(t) = \frac{1}{C} \int_0^t i(\tau) d\tau + v_{C0}$$

- Mathematic model

$$(4.2.2-2) \quad i_R(t) = i_L(t) = i_C(t) = i(t)$$

$$(4.2.2-3) \quad v_R(t) + v_L(t) + v_C(t) = Ri(t) + Li'(t) + \frac{1}{C} \int_0^t i(\tau) d\tau + v_{C0} = v_s(t)$$

$$\Rightarrow R\hat{i}(s) + sL\hat{i}(s) - Li_{Lo} + \frac{1}{sC}\hat{i}(s) + \frac{v_{C0}}{s} = \frac{s}{s^2 + \omega^2}$$

Hence, we have

$$(4.2.2-4) \quad \hat{i}(s) = \frac{s^3 i_{Lo} + s i_{Lo} \omega^2 + \frac{1-v_{C0}}{L} s^2 - \frac{v_{C0}}{L} \omega^2}{\left(s^2 + \frac{R}{L}s + \frac{1}{LC}\right)(s^2 + \omega^2)}$$

$$= \frac{\Psi(s)}{(s^2 + 2\alpha s + \omega_0^2)(s^2 + \omega^2)} = \frac{\Psi(s)}{(s^2 + 2\xi\omega_0 s + \omega_0^2)(s^2 + \omega^2)}$$

where $\Psi(s) = s^3 i_{Lo} + s i_{Lo} \omega^2 + \frac{1-v_{C0}}{L} s^2 - \frac{v_{C0}}{L} \omega^2$, $\alpha = \frac{R}{2L}$, $\omega_0 = \frac{1}{\sqrt{LC}}$ and

$$\xi = \frac{\alpha}{\omega_0} = \frac{R}{2} \sqrt{\frac{C}{L}}$$

- Characteristic roots λ_1 , λ_2 and $\pm j\omega$

Let $(s^2 + 2\xi\omega_0 s + \omega_0^2)(s^2 + \omega^2) = (s - \lambda_1)(s - \lambda_2)(s^2 + \omega^2)$, then

$$(4.2.2-5) \quad \hat{i}(s) = \frac{\Psi(s)}{(s^2 + 2\xi\omega_0 s + \omega_0^2)(s^2 + \omega^2)} = \frac{\Psi(s)}{(s - \lambda_1)(s - \lambda_2)(s^2 + \omega^2)}$$

where $\lambda_1, \lambda_2 = (-\xi \pm \sqrt{\xi^2 - 1})\omega_0$.

- [A] $\xi = \frac{R}{2} \sqrt{\frac{C}{L}} > 1$

That means $\lambda_2 < \lambda_1 < 0$ and

$$(4.2.2-6) \quad \hat{i}(s) = \frac{\Psi(s)}{(s - \lambda_1)(s - \lambda_2)(s^2 + \omega^2)} = \frac{A_1}{s - \lambda_1} + \frac{A_2}{s - \lambda_2} + \frac{A_3 s + A_4 \omega}{s^2 + \omega^2}$$

$$\Rightarrow i(t) = A_1 e^{\lambda_1 t} + A_2 e^{\lambda_2 t} + A_3 \cos \omega t + A_4 \sin \omega t$$

where $A_1 = \frac{\Psi(\lambda_1)}{(\lambda_1 - \lambda_2)(\lambda_1^2 + \omega^2)}$, $A_2 = \frac{\Psi(\lambda_2)}{(\lambda_2 - \lambda_1)(\lambda_2^2 + \omega^2)}$,

$$A_3 - jA_4 = \frac{\Psi(j\omega)}{\omega^2(\lambda_1 + \lambda_2) + j\omega(\lambda_1 \lambda_2 - \omega^2)}.$$

- [B] $\xi = \frac{R}{2} \sqrt{\frac{C}{L}} = 1$

That means $\lambda_2 = \lambda_1 = -\xi \omega_0 = -\alpha$ and

$$(4.2.2-7) \quad \hat{i}(s) = \frac{\Psi(s)}{(s + \alpha)^2(s^2 + \omega^2)} = \frac{B_1}{s + \alpha} + \frac{B_2}{(s + \alpha)^2} + \frac{B_3 s + B_4 \omega}{s^2 + \omega^2}$$

$$\Rightarrow i(t) = (B_1 + B_2 t) e^{-\alpha t} + B_3 \cos \omega t + B_4 \sin \omega t$$

where $B_2 = \frac{\psi(-\alpha)}{\alpha^2 + \omega^2}$, $B_1 = \frac{\psi'(-\alpha) - 2\alpha B_2}{\alpha^2 + \omega^2}$,

$$B_3 - jB_4 = \frac{\Psi(j\omega)}{-2\alpha\omega^2 + j\omega(\alpha^2 - \omega^2)}.$$

- [C] $\xi = \frac{R}{2} \sqrt{\frac{C}{L}} < 1$

That means $\lambda_1, \lambda_2 = \left(-\xi \pm j\sqrt{1 - \xi^2} \right) \omega_0 = -\alpha \pm j\beta$ and

$$(4.2.2-8) \quad \hat{i}(s) = \frac{\psi(s)}{(s^2 + 2\xi\omega_0 s + \omega_0^2)(s^2 + \omega^2)} = \frac{(s + \alpha)D_1 + \beta D_2}{(s + \alpha)^2 + \beta^2} + \frac{sD_3 + \omega D_4}{s^2 + \omega^2}$$

$$\Rightarrow i(t) = e^{-\alpha t} (D_1 \cos \beta t + D_2 \sin \beta t) + D_3 \cos \omega t + D_4 \sin \omega t$$

where $D_1 - jD_2 = \frac{\psi(-\alpha + j\beta)}{2\alpha\beta^2 + j\beta(\alpha^2 - \beta^2 + \omega^2)}$,

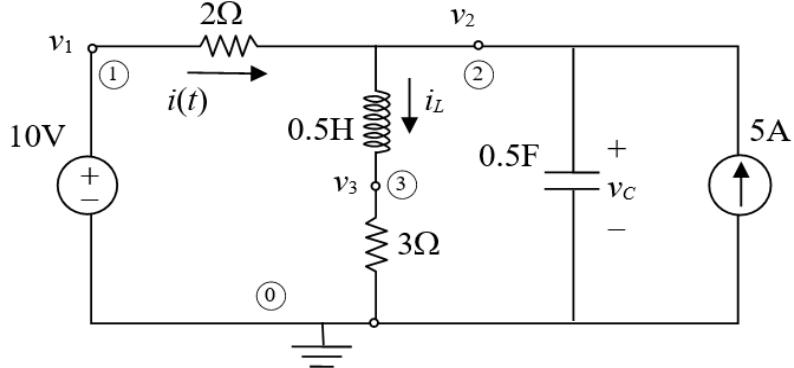
$$D_3 - jD_4 = \frac{\psi(j\omega)}{-2\alpha\omega^2 + j\omega(\alpha^2 + \beta^2 - \omega^2)}.$$

- From (4.2.2-1) and $i(t)$, we can obtain the currents through R , L and C .

Example: Consider a second-order series RLC circuit with voltage source $v_s(t) = \sin 2t$ V. If $R = 4 \Omega$, $L = 2 \text{ H}$, and $C = 0.125 \text{ F}$, determine $i(t)$ and $v_L(t)$ for $t \geq 0$ when $v(0) = 1 \text{ V}$ and $i(0) = -1 \text{ A}$.

4.3 General linear RLC circuits

Example: Given $i_L(0) = 2 \text{ A}$ and $v_C(0) = 6 \text{ V}$, determine $i(t)$ for $t \geq 0$.



Node voltage equations:

$$\text{KVL } ①: v_1 = 10$$

$$\text{KCL } ②: \frac{1}{2}(v_2 - v_1) + i_L + i_C - 5$$

$$= \frac{1}{2}(v_2 - v_1) + \frac{1}{0.5} \int_0^t (v_2 - v_3) d\tau + 2 + 0.5v'_2 - 5 = 0$$

$$\text{KCL } ③: -i_L + \frac{v_3}{3} = -\left(\frac{1}{0.5} \int_0^t (v_2 - v_3) d\tau + 2\right) + \frac{v_3}{3} = 0$$

Taking Laplace transform yields

$$\text{KVL } ①: \hat{v}_1(s) = \frac{10}{s}$$

$$\text{KCL } ②: 0.5(\hat{v}_2(s) - \hat{v}_1(s)) + \frac{2}{s}(\hat{v}_2(s) - \hat{v}_3(s)) + \frac{2}{s}$$

$$+ 0.5(s\hat{v}_2(s) - 6) - \frac{5}{s} = 0$$

$$\text{KCL } ③: -\left(\frac{2}{s}(\hat{v}_2(s) - \hat{v}_3(s)) + \frac{2}{s}\right) + \frac{\hat{v}_3(s)}{3} = 0$$

i.e.,

$$(4.3-1) \quad \hat{v}_1(s) = \frac{10}{s}$$

$$(4.3-2) \quad -s\hat{v}_1(s) + (s^2 + s + 4)\hat{v}_2(s) - 4\hat{v}_3(s) = 6s + 6$$

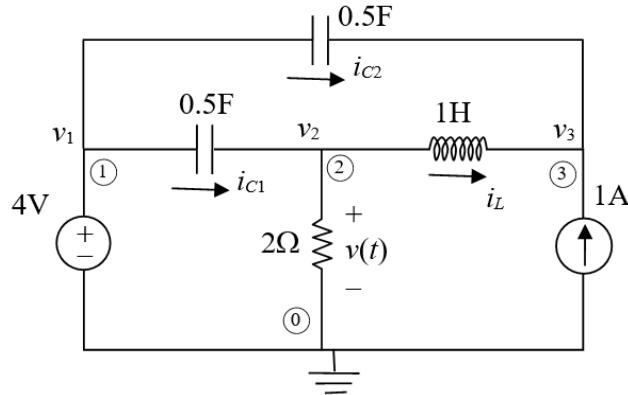
$$(4.3-3) \quad -6\hat{v}_2(s) + (s + 6)\hat{v}_3(s) = 6$$

$$\text{Hence, } \hat{v}_1(s) = \frac{10}{s}, \quad \hat{v}_2(s) = \frac{6s^2 + 52s + 120}{s(s^2 + 7s + 10)}, \quad \hat{v}_3(s) = \frac{6s^2 + 42s + 120}{s(s^2 + 7s + 10)}$$

$$\text{and } \hat{i}(s) = \frac{1}{2}(\hat{v}_1(s) - \hat{v}_2(s)) = \frac{-1}{s} + \frac{10/3}{s+2} + \frac{-1/3}{s+5}$$

$$\text{The current is } i(t) = -1 + \frac{10}{3}e^{-2t} - \frac{1}{3}e^{-5t}, \quad t \geq 0.$$

Example: If $i_L(0) = 1\text{A}$ and there are no initial capacitor voltages, determine $v(t)$ for $t \geq 0$.



Node voltage equations:

$$\text{KVL } \textcircled{1}: \quad v_1 = 4$$

$$\text{KCL } \textcircled{2}: \quad \frac{1}{2}v_2 - i_{C1} + i_L = \frac{1}{2}v_2 - 0.5(v'_1 - v'_2) + \int_0^t (v_2 - v_3) d\tau + 1 = 0$$

$$\text{KCL } \textcircled{3}: \quad i_L + i_{C2} + 1 = \int_0^t (v_2 - v_3) d\tau + 1 + 0.5(v'_1 - v'_3) + 1 = 0$$

Taking Laplace transform yields

$$\text{KVL } \textcircled{1}: \quad \hat{v}_1(s) = \frac{4}{s}$$

$$\text{KCL } \textcircled{2}: \quad \frac{1}{2}\hat{v}_2(s) - 0.5s(\hat{v}_1(s) - \hat{v}_2(s)) + \frac{1}{s}(\hat{v}_2(s) - \hat{v}_3(s)) + \frac{1}{s} = 0$$

$$\text{KCL } \textcircled{3}: \quad \frac{1}{s}(\hat{v}_2(s) - \hat{v}_3(s)) + \frac{1}{s} + 0.5s(\hat{v}_1(s) - \hat{v}_3(s)) + \frac{1}{s} = 0$$

i.e.,

$$(4.3-1) \quad \hat{v}_1(s) = \frac{10}{s}$$

$$(4.3-2) \quad s^2\hat{v}_1(s) - (s^2 + s + 2)\hat{v}_2(s) + 2\hat{v}_3(s) = 2$$

$$(4.3-3) \quad s^2\hat{v}_1(s) + 2\hat{v}_2(s) - (s^2 + 2)\hat{v}_3(s) = -4$$

It can be obtained that $\hat{v}_2(s) = \frac{10s^3 - 2s^2 + 40s + 4}{s(s^3 + s^2 + 4s + 2)}$.

Since $v(t) = v_2(t)$, we have

$$(4.3-4) \quad \begin{aligned} \hat{v}(s) &= \frac{10s^3 - 2s^2 + 40s + 4}{s(s^3 + s^2 + 4s + 2)} \\ &= \frac{A}{s} + \frac{B}{s + 0.5332} + \frac{(s + 0.2334)C + 1.9227D}{(s + 0.2334)^2 + 1.9227^2} \end{aligned}$$

Once A, B, C and D are solved, the voltage is expressed as

$$(4.3-5) \quad v(t) = A + Be^{-0.5332t} + e^{-0.2334t} (C \cos 1.9227t + D \sin 1.9227t).$$